



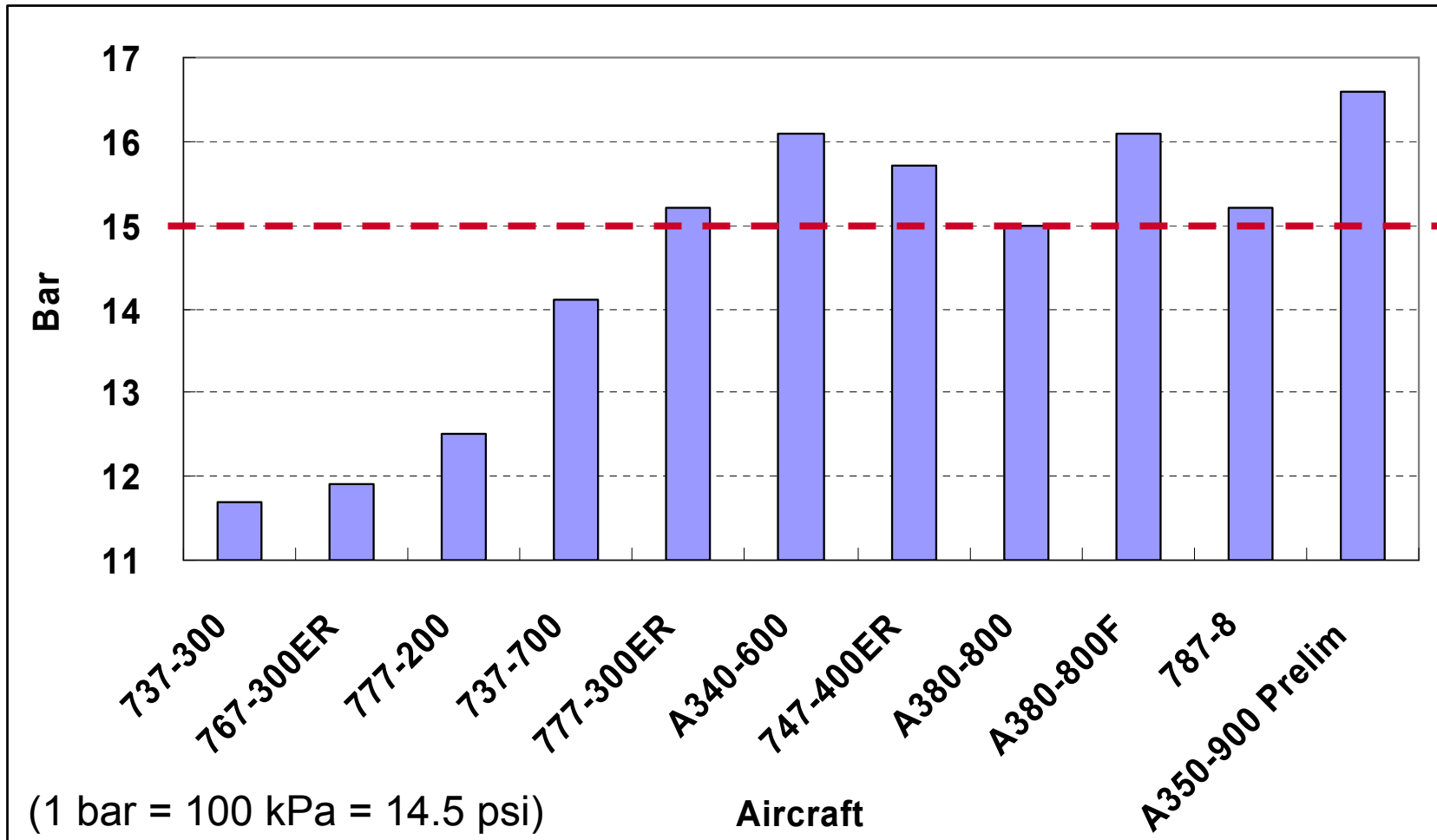
Simulation of NAPTF High Tire Pressure Tests with Advanced Finite Element Modeling

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Aircraft Tire Pressure Trend



(After C. Fabre, 2009)

Objective and Scope

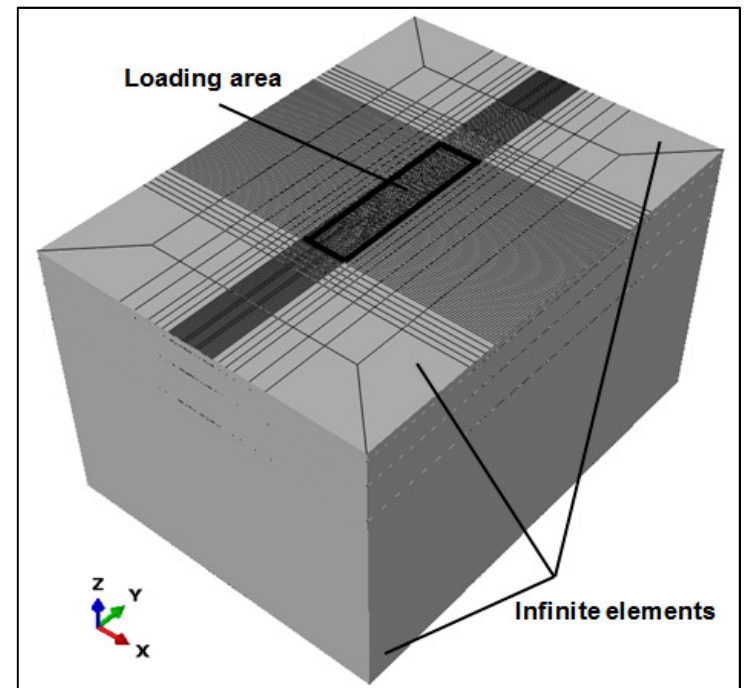
- ❑ **Develop a 3-D viscoelastic finite element model for airfield pavement test sections at NAPTF**
- ❑ **Evaluate effect of aircraft tire pressure on pavement responses and rutting using different temperature profiles**
 - 1.45MPa (210psi) vs. 1.69MPa (245psi)

Calculation of Pavement Response

- **Layered Elastic Theory**
 - ❑ Simple loading and material assumption
 - ❑ Public software available
 - ❑ Fast computation speed
- **Finite Element Method**
 - ❑ Complex loading condition and material properties
 - ❑ Flexible geometry and discontinuities (joint, crack, interface, interlayer, et al.)
 - ❑ Large computation resource and time

3-D FE Pavement Modeling

- ❑ Moving tire load with pre-defined contact area and stress
- ❑ Quasi-static or dynamic analysis
- ❑ Viscoelastic asphalt layer
- ❑ Nonlinear anisotropic unbound layer
- ❑ Frictional interface



Element Size and Boundary Conditions

- ❑ **Element vertical size:**

- ❑ 12.7 mm for HMA layer
- ❑ 40-50 mm for base layer

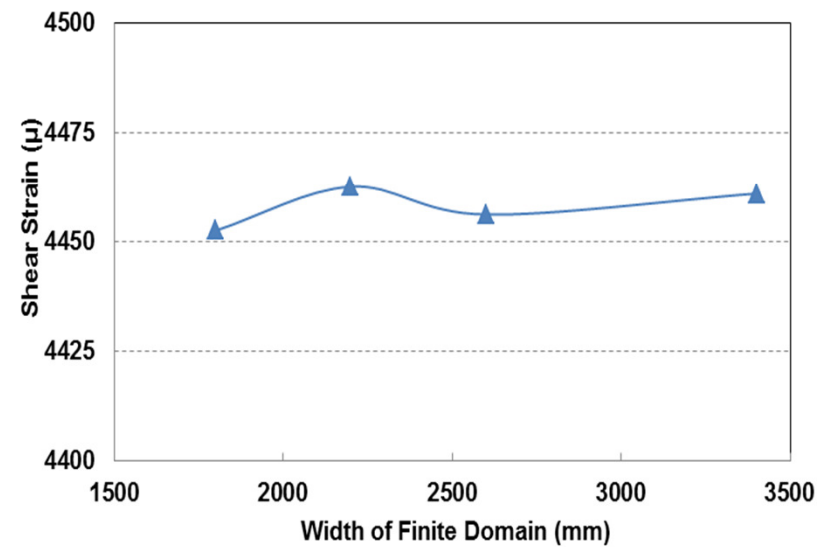
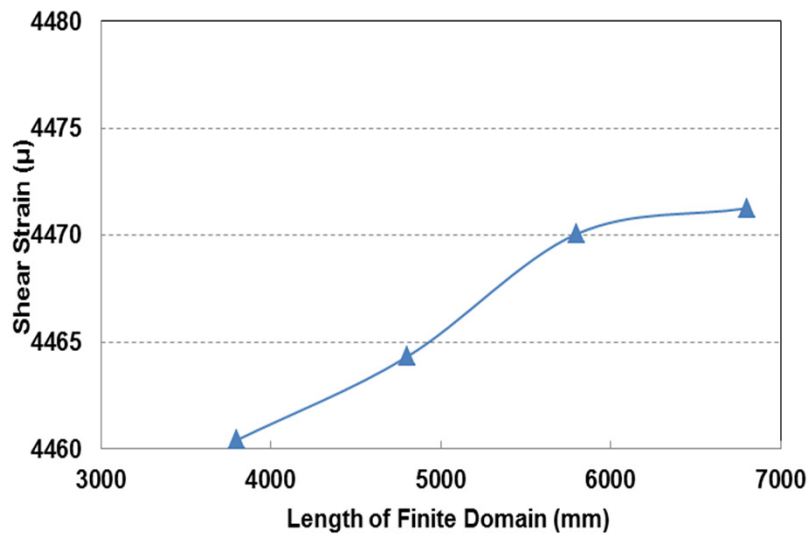
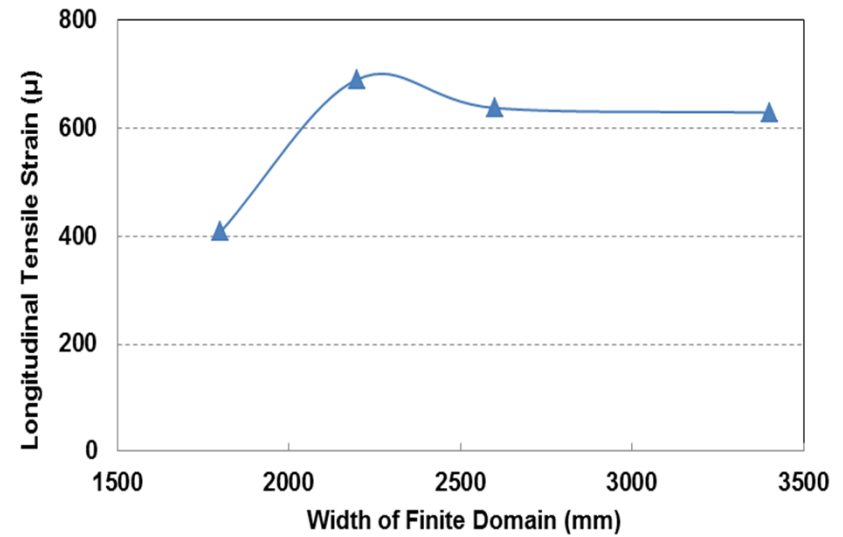
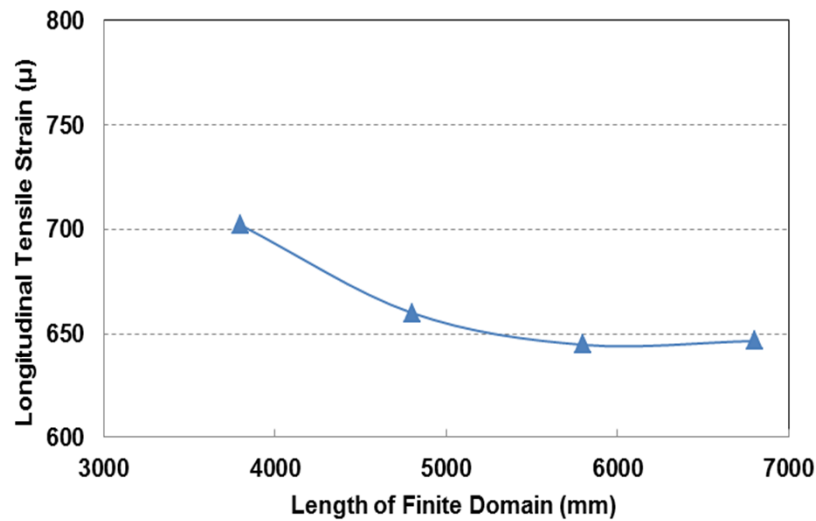
- ❑ **Element horizontal dimension:**

- ❑ 10-20 mm in the transverse direction
- ❑ 40 mm in the longitudinal (moving) direction

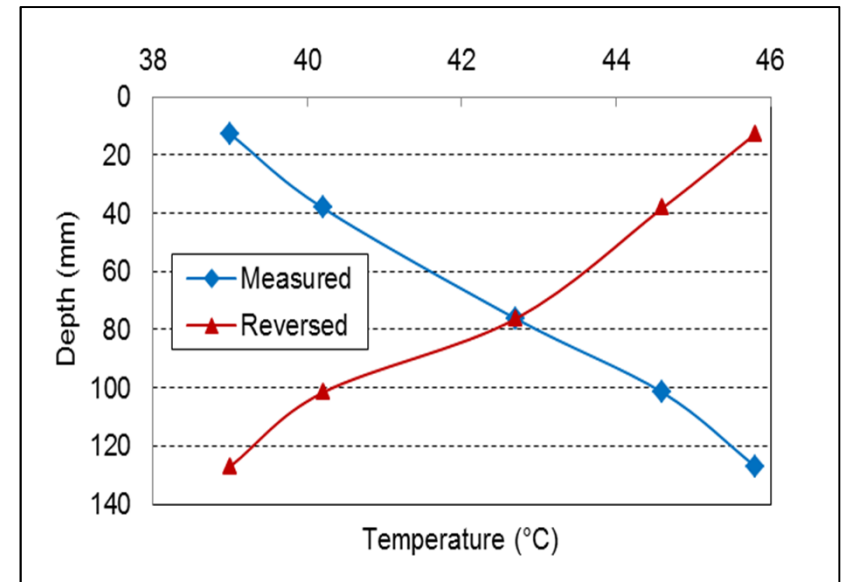
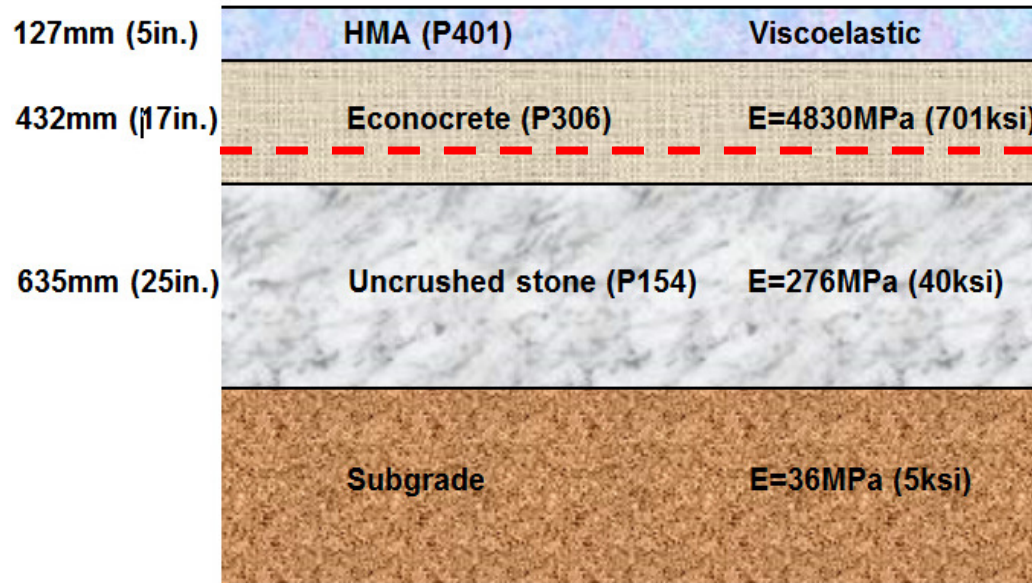
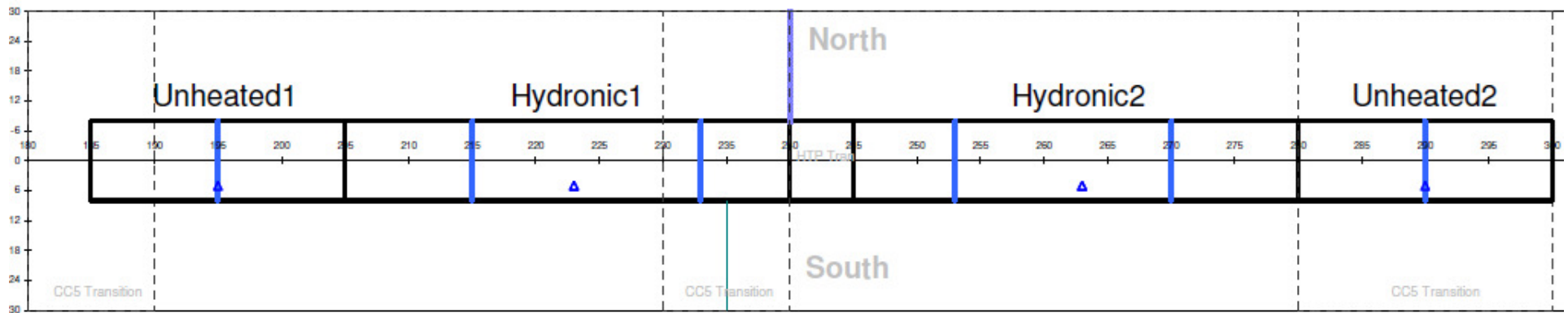
- ❑ **Infinite elements used to reduce degrees of freedom and create “silent” boundaries**

- ❑ **Coulomb frictional interfaces are used**

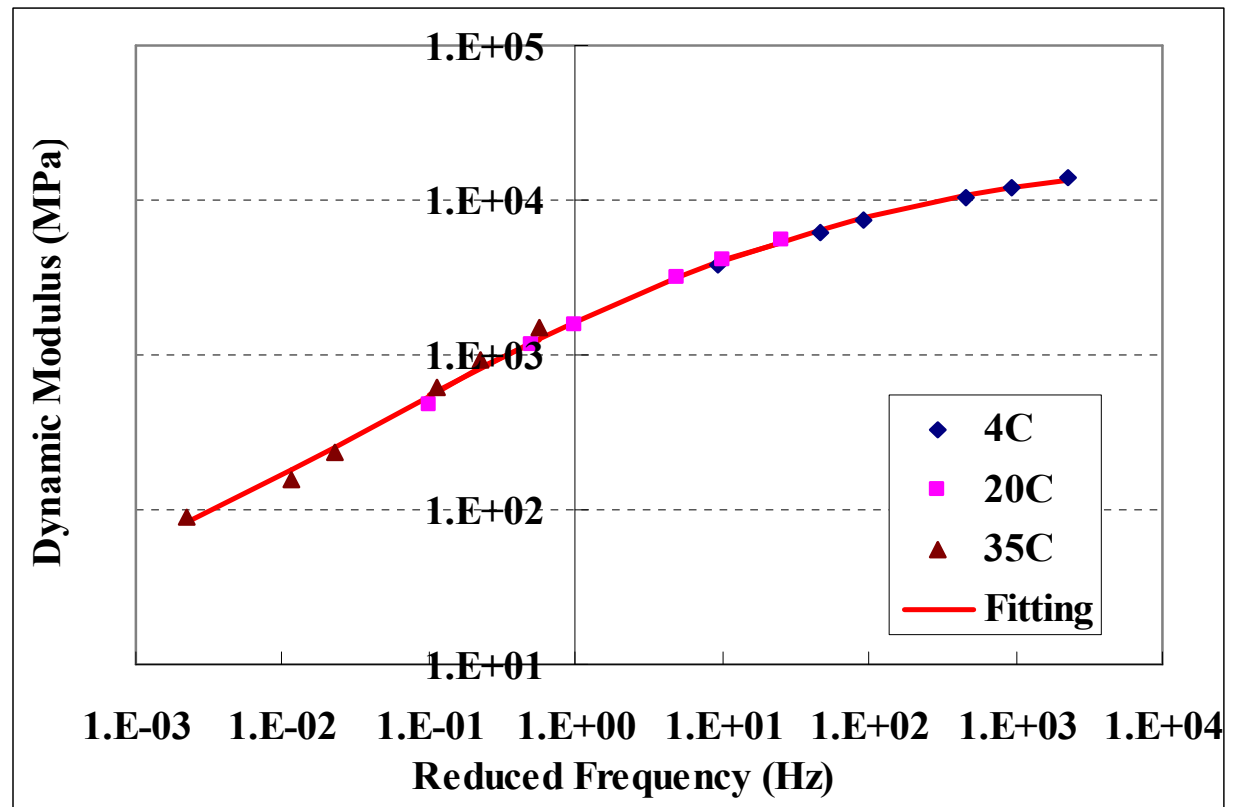
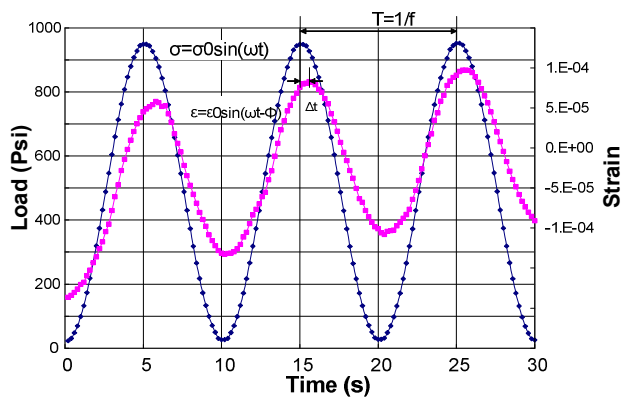
Determination of FE Model Size



Pavement Structure



Material Characterization



HMA Linear Viscoelasticity

- Generalized Maxwell Solid Model: Consists of one spring and n Maxwell elements connected in parallel**

$$E(t) = E_0 \left(1 - \sum_{i=1}^N E_i (1 - e^{-t/\tau_i}) \right)$$

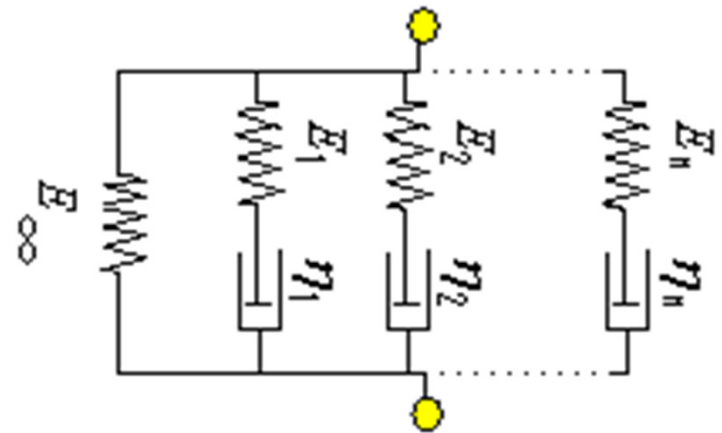
where,

$E(t)$ is relaxation modulus;

E_0 is instantaneous modulus;

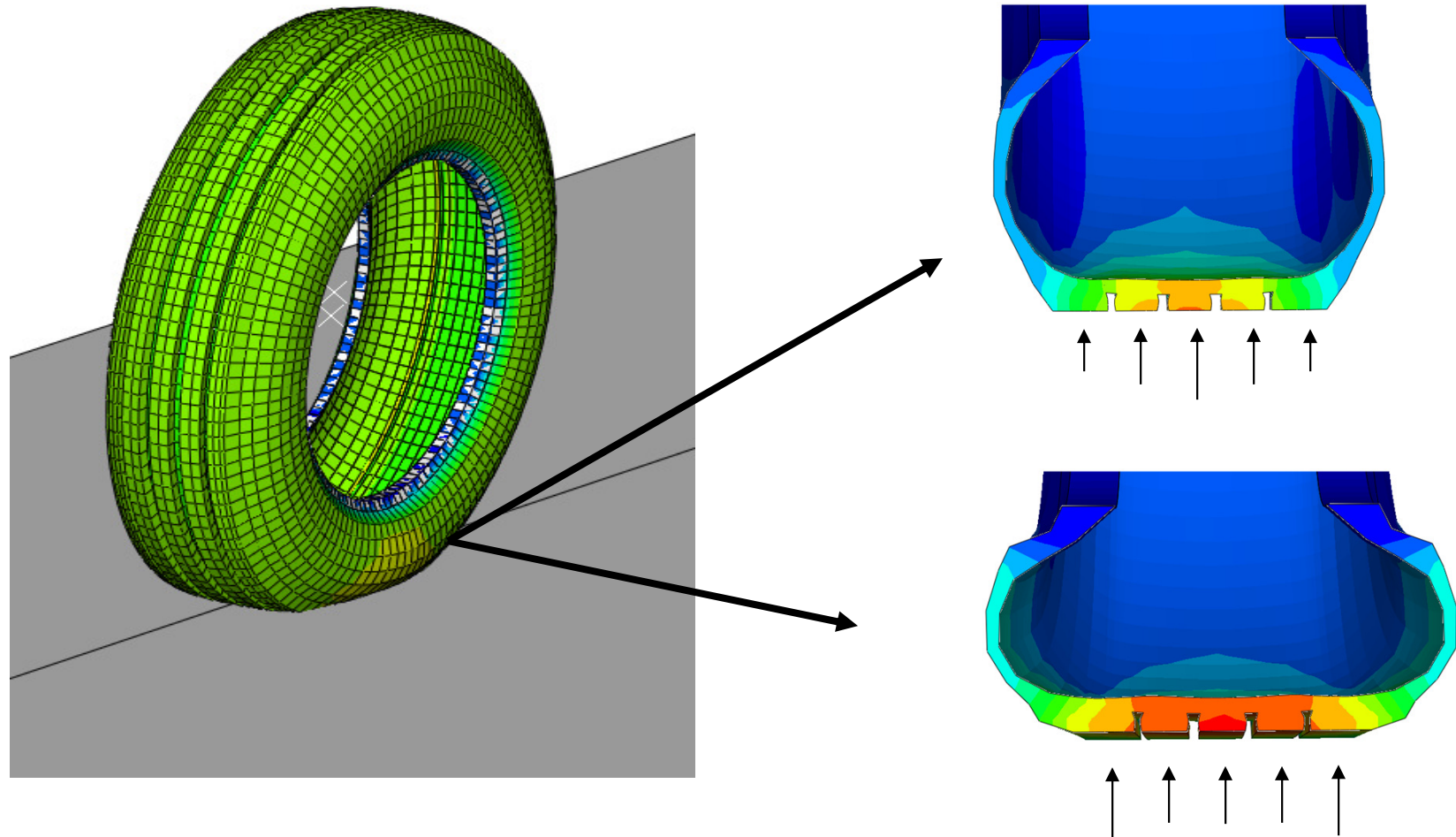
E_i and τ_i are Prony series parameters; and

t is relaxation time.



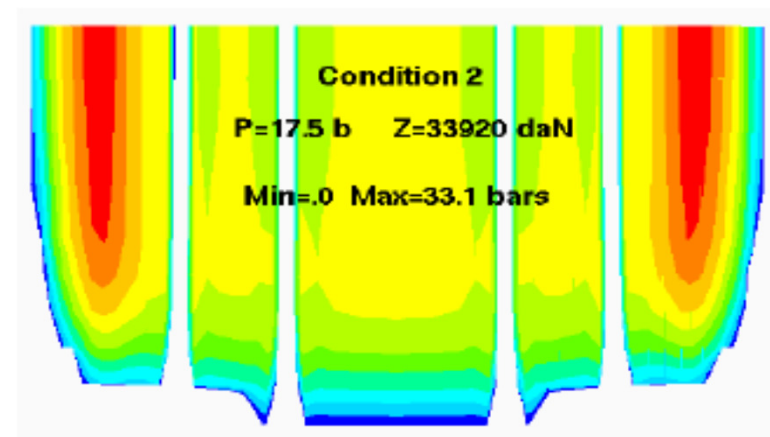
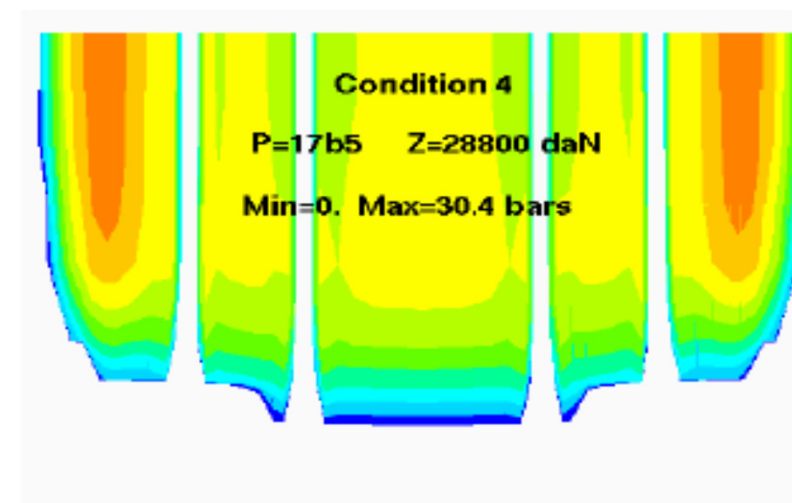
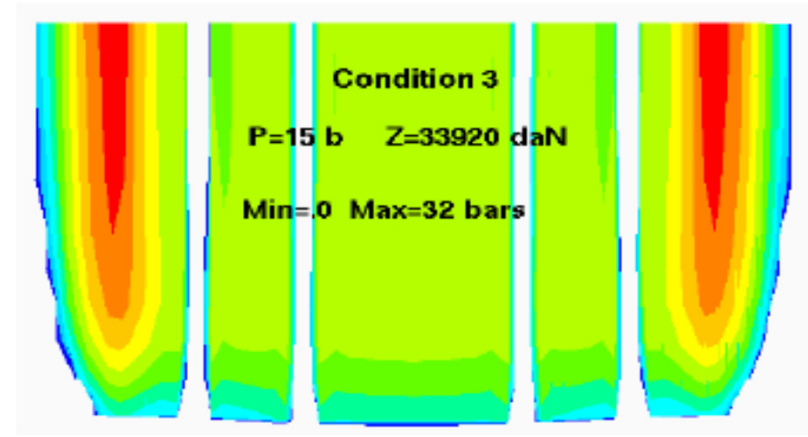
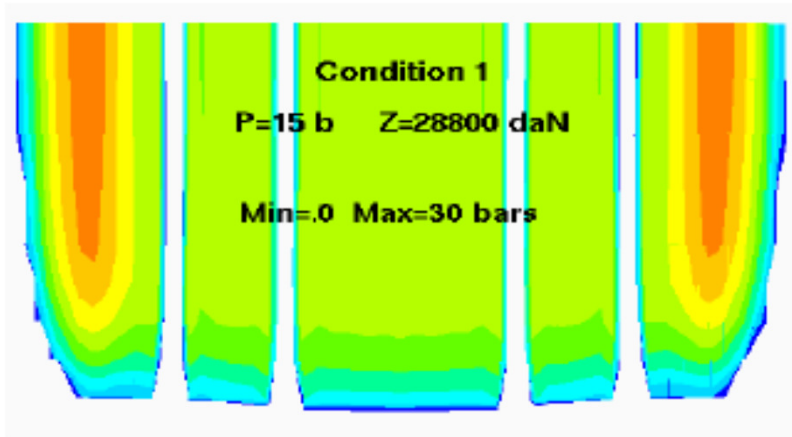
- Relaxation modulus is converted from dynamic modulus and expressed as Prony Series**

Non-Uniform Tire Contact Stress



Wang, H., I.L. Al-Qadi, and I. Stanciulescu, Simulation of Tire-Pavement Interaction for Predicting Contact Stresses at Static and Rolling Conditions,. International Journal of Pavement Engineering, Vol. 13, No.4, 2012, pp. 310-321

Changes in Tire Contact Pressure under Aircraft Load



100daN = 1kN = 0.225kip

1 Bar = 100kPa = 14.5psi

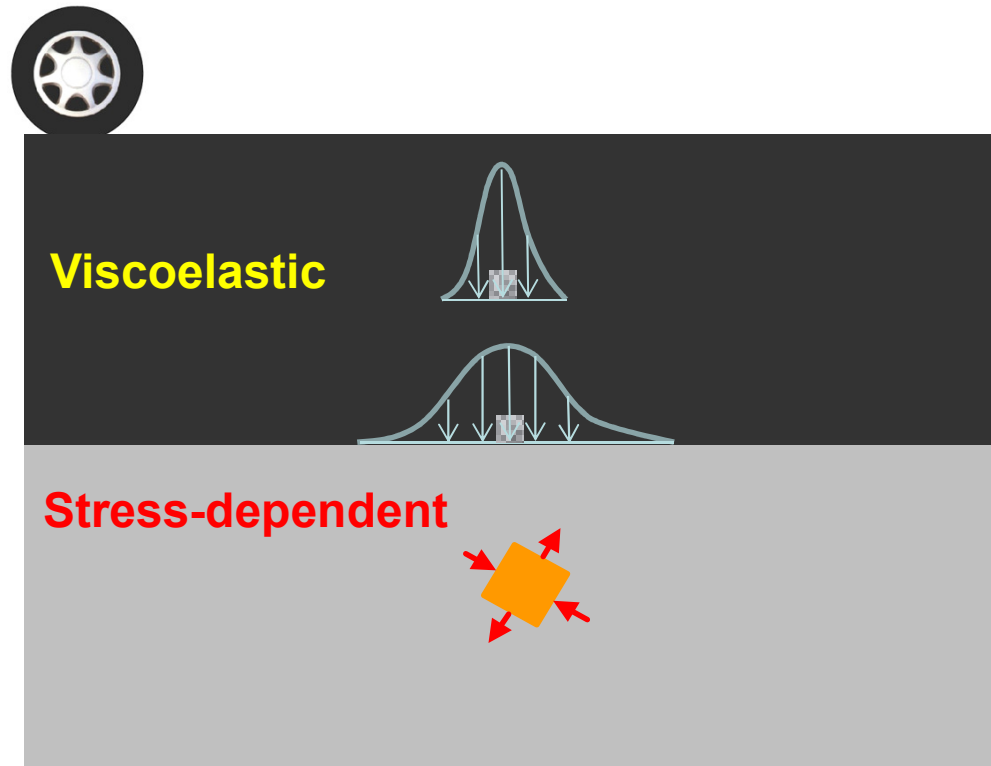
(After E. Rolland, Michelin)

Non-uniform Pressure Distribution

(1.69MPa and 1.45MPa)

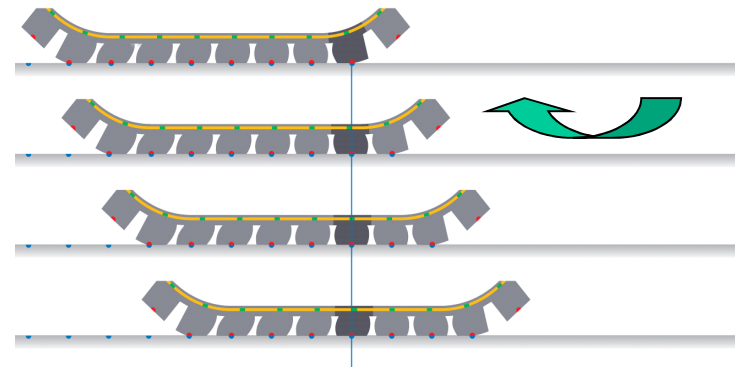
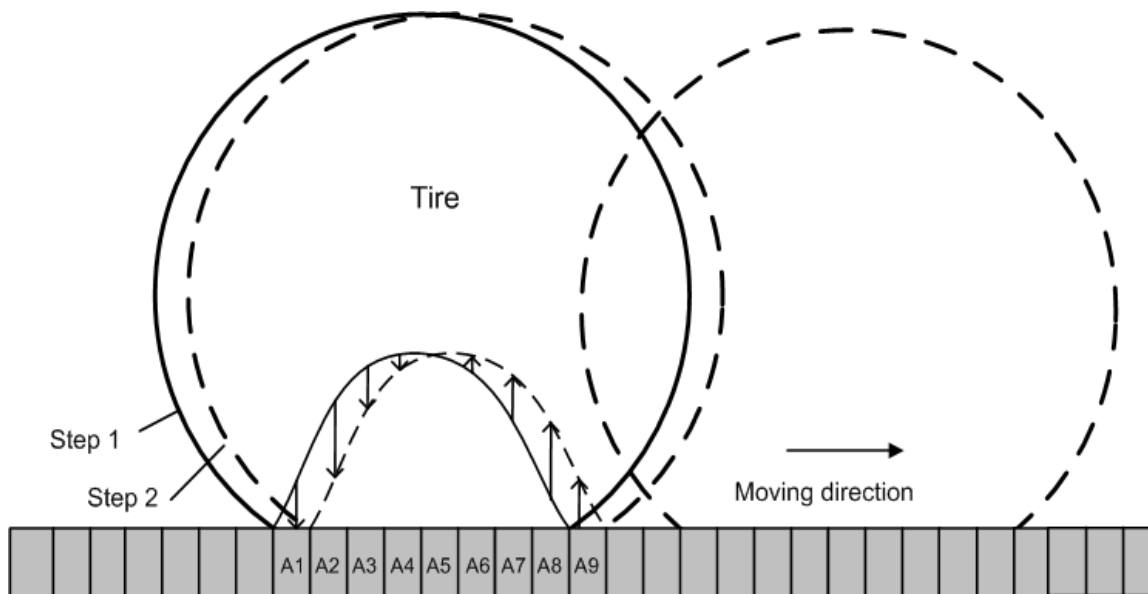
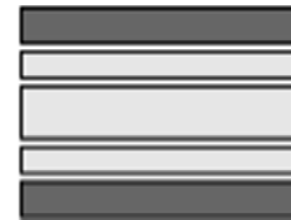
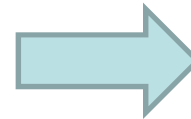
Contact pressure assumptions		Contact width (mm)	Contact length (mm)	Peak pressure (MPa)
Non-uniform	Rib 1	60	440 / 520	4.23 / 3.63
	Rib 2	50	440 / 520	2.11 / 1.74
	Rib 3	120	440 / 520	2.11 / 1.74
	Rib 4	50	440 / 520	2.11 / 1.74
	Rib 5	60	440 / 520	4.23 / 3.63
	Groove	15	440 / 520	0

Importance of Moving Load

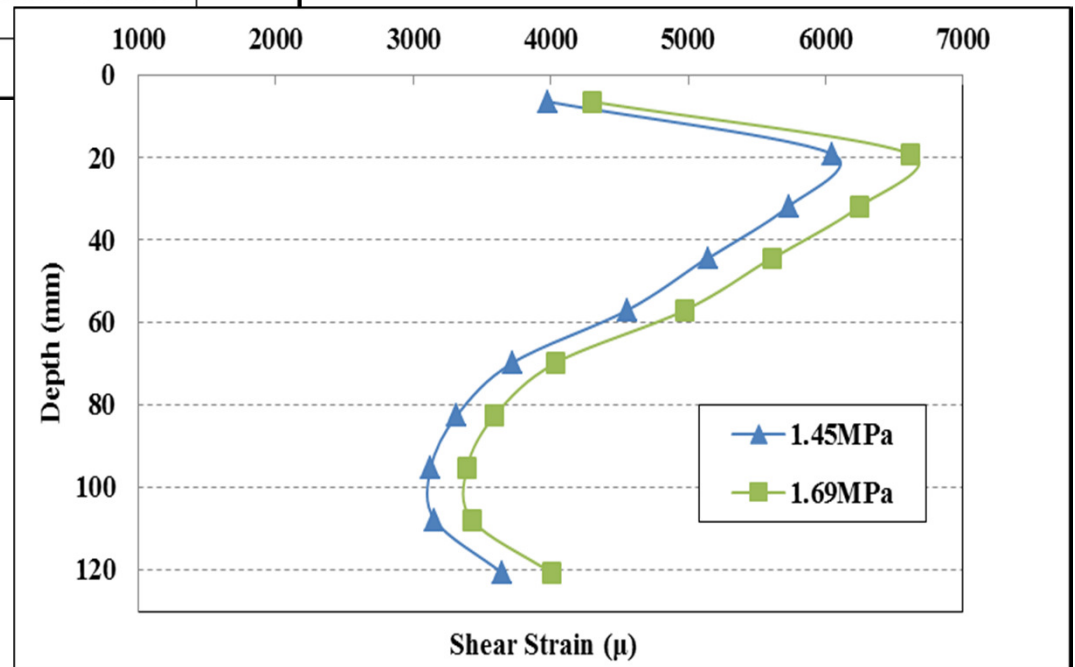
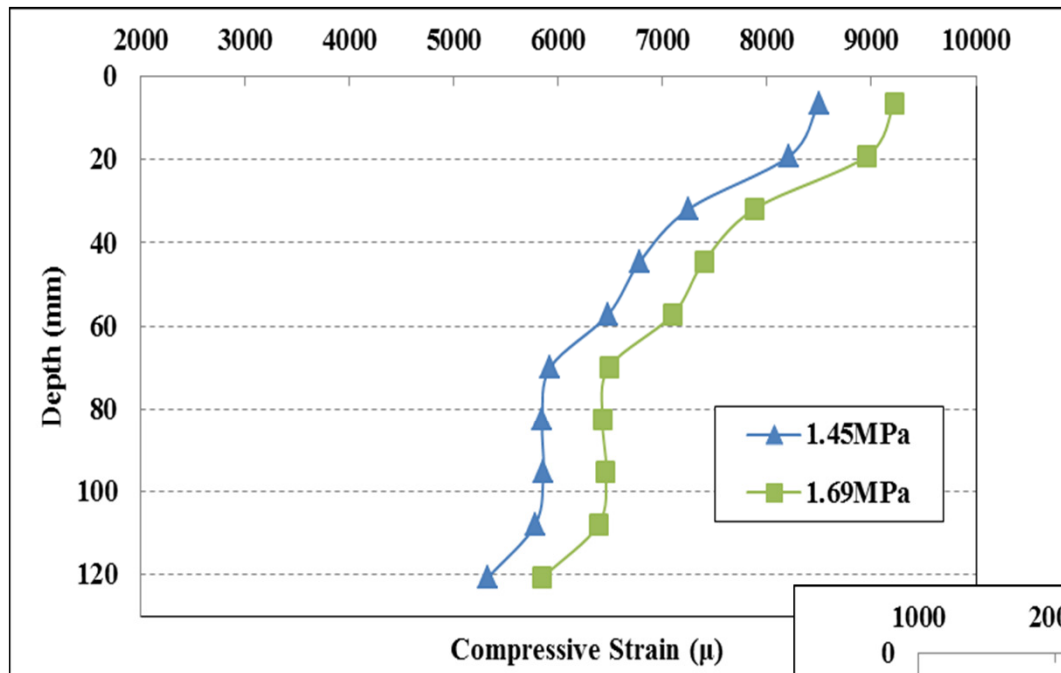


- ❑ **Loading time varies** at various pavement depths and directions
- ❑ **Principal stresses rotate** under a moving load

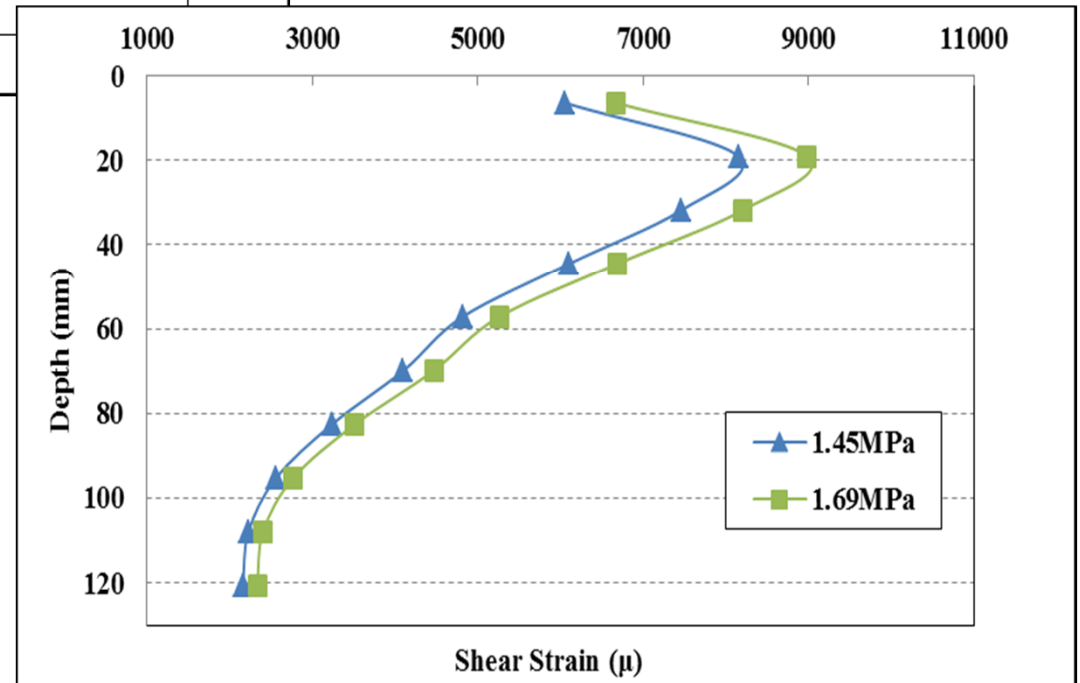
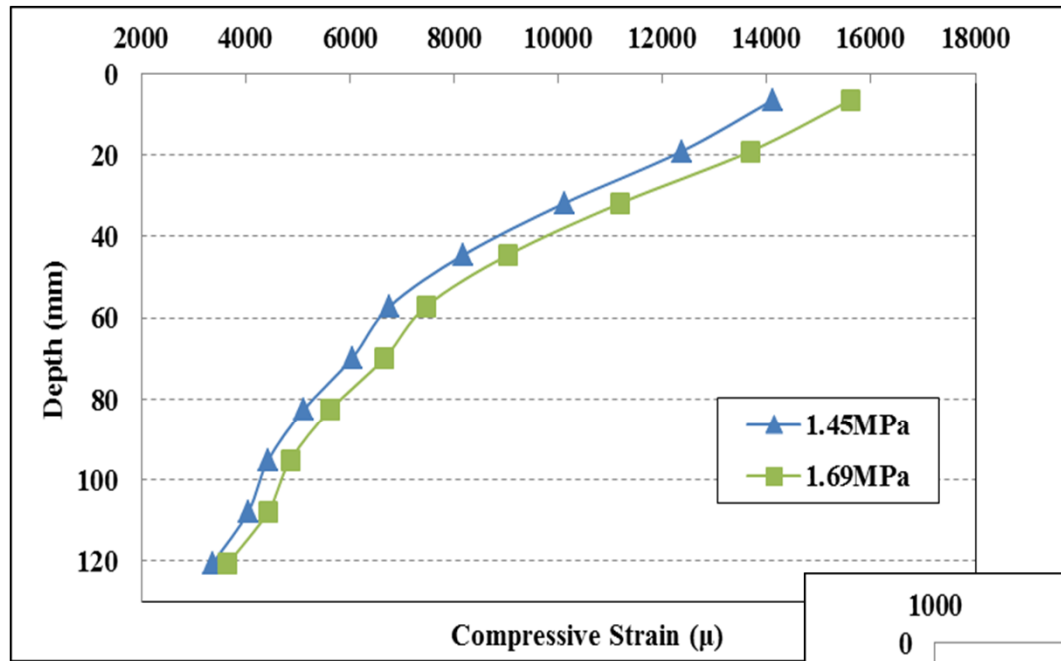
Simulation of Tire Loading



In-depth Strain Distribution (measured temperature profile at NAPTF)



In-depth Strain Distribution (reversed temperature profile at NAPTF)



Effect of Tire Pressure on Responses

Tire load: 272.7kN (61.3kips)	Measured Temperature Profile			Reversed Temperature Profile		
Tire pressure (MPa)	1.45	1.69	Change	1.45	1.69	Change
Critical tensile strain (μ)	1068	1339	+25%	899	1101	+22%
Shear strain (μ)	6049	6617	+9%	8158	8891	+10%
Compressive strain (μ)	8496	9225	+9%	14119	15614	+11%
Deviator Stress (kPa)	2107	2489	+18%	1823	2154	+18%

Calculation of Rutting Depth (MEPDG)

$$\frac{\varepsilon_p}{\varepsilon_r} = k_1 * 10^{-3.4488} T^{1.5606} N^{0.479244}$$

$$k_1 = (C_1 + C_2 * depth) * 0.328196^{depth}$$

$$C_1 = -0.1039 * h_{ac}^2 + 2.4868 * h_{ac} - 17.342$$

$$C_2 = 0.0172 * h_{ac}^2 - 1.7331 * h_{ac} + 27.428$$

where,

k_1 = function of total asphalt layers thickness (h_{ac} , in) and depth ($depth$, in) to computational point, to correct for the confining pressure at different depths

$$RD_{AC} = \sum_{i=1}^N (\varepsilon_p)_i \cdot \Delta h_i$$

RD_{AC}	= rut depth at the asphalt concrete layer
N	= number of sublayers
$(\varepsilon_p)_i$	= vertical plastic strain at mid-thickness of layer i
Δh_i	= thickness of sublayer i

Calculation of Rutting Depth (AI)

$$\begin{aligned} \text{Log}\left(\frac{\epsilon_p}{\epsilon_r}\right) = & -6.631 + 0.4354\text{Log}(N) + 2.767\text{Log}(T) \\ & + 0.110\text{Log}(\sigma_d) - 0.118\text{Log}(\eta) \\ & + 0.930\text{Log}(V_{beff}) + 0.501\text{Log}(V_a) \end{aligned}$$

where

σ_d = deviator stress, psi.

η = viscosity of the asphalt binder at 70°F, $\times 10^6$ poise.

V_{beff} = effective asphalt content by volume, percent.

V_a = air void volume, percent.

$$RD_{AC} = \sum_{i=1}^N (\epsilon_p)_i \cdot \Delta h_i$$

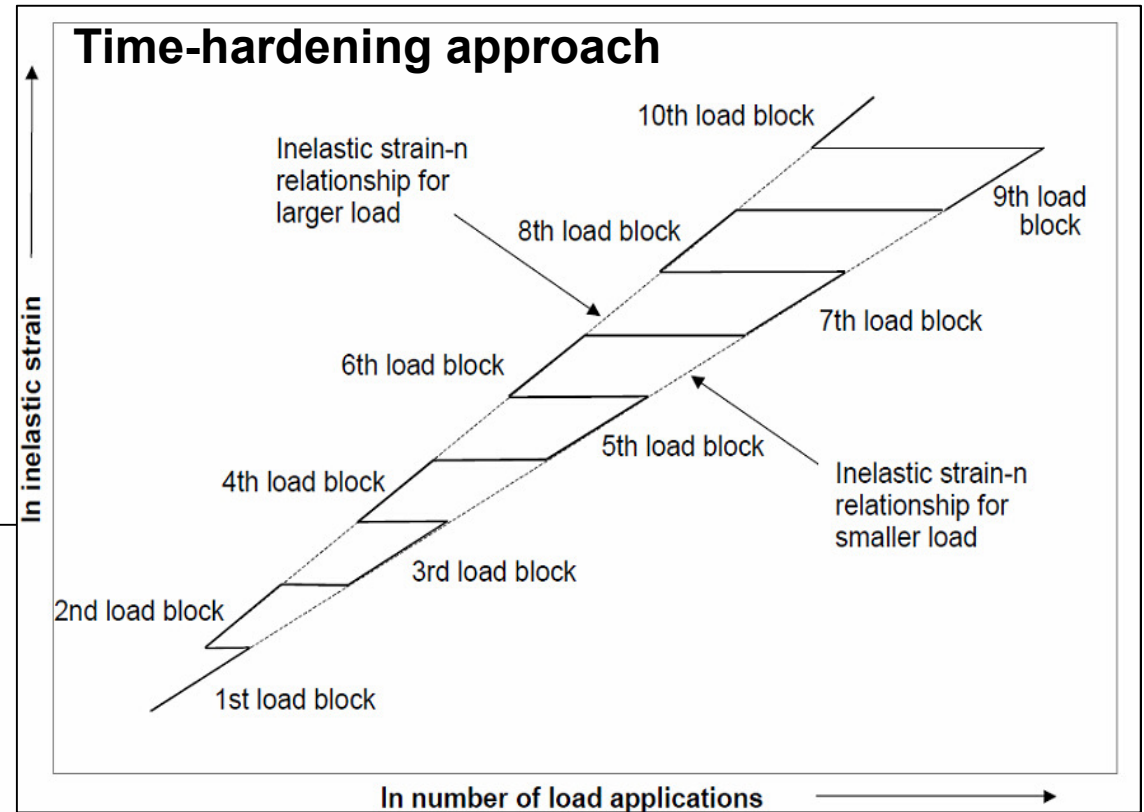
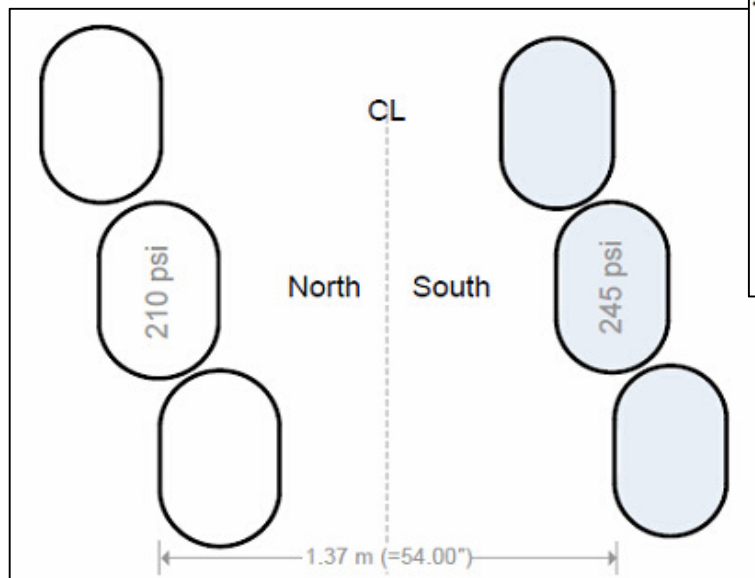
RD_{AC}	= rut depth at the asphalt concrete layer
N	= number of sublayers
$(\epsilon_p)_i$	= vertical plastic strain at mid-thickness of layer i
Δh_i	= thickness of sublayer i

Effect of Tire Pressure on Rutting Depth

Tire load: 272.7kN (61.3kips)	AI Model			MEPDG model		
Tire pressure: Mpa (psi)	1.45 (210)	1.69 (245)	Change	1.45 (210)	1.69 (245)	Change
Rut depth (in.)	Measured temperature profile at NAPTF					
400th cycle	1.40	1.56	+11%	0.65	0.71	+9%
800th cycle	1.90	2.11	+11%	0.91	1.00	+10%
Rut depth (in.)	Reversed temperature profile					
400th cycle	1.55	1.74	+12%	0.77	0.85	+10%
800th cycle	2.09	2.35	+12%	1.08	1.19	+10%

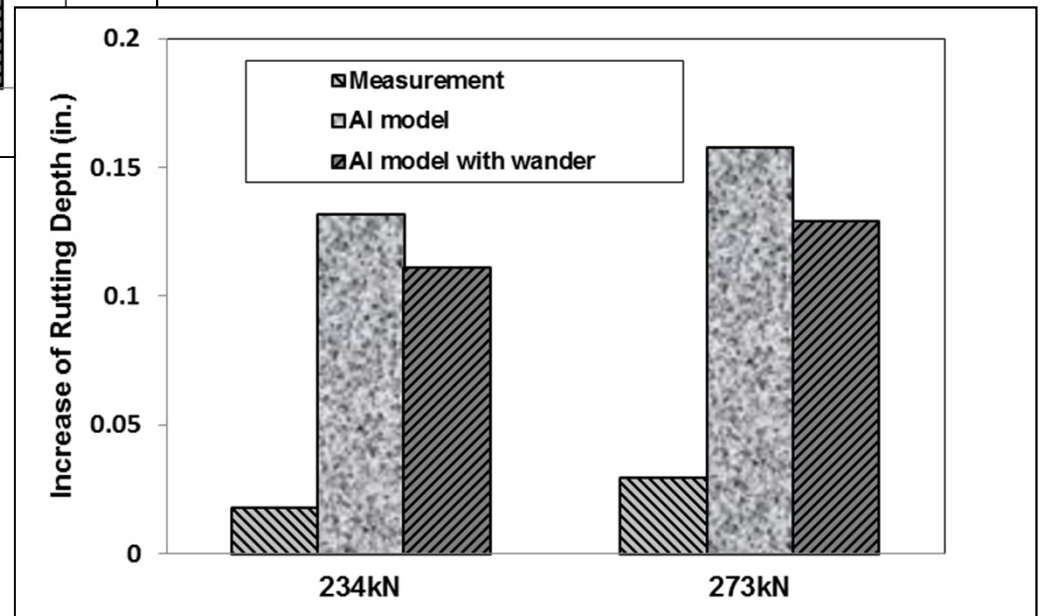
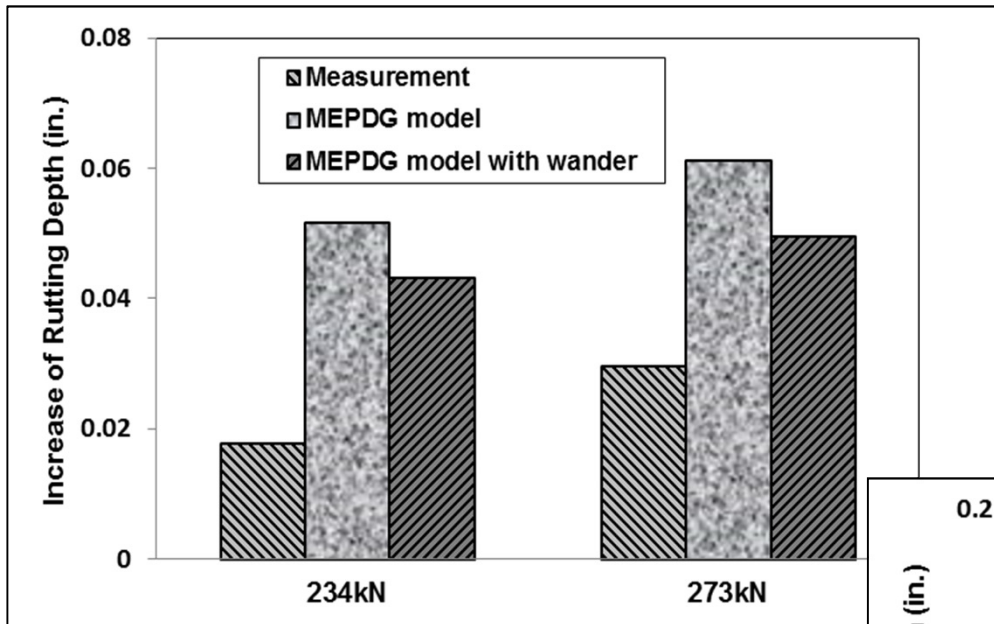
Simulation of Wander Pattern

Wander during APT



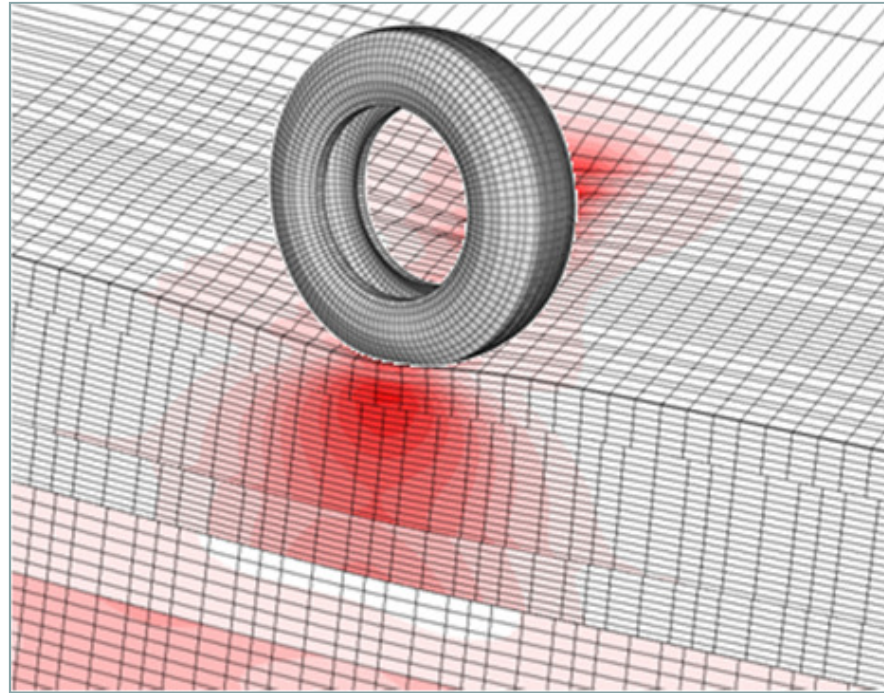
(After Monismith et al. 2006)

Effect of Wandering on Rutting



Conclusions

- **The high tire pressure causes greater responses by different percentages**
 - Temperature profile affects maximum pavement responses
 - Changes of maximum strain responses due to tire pressure are not affected by temperature variation
- **The high tire pressure causes slightly greater rutting depth**
 - Calibration is needed to predict accurate rutting depth



**Thank You
Questions ?**

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